

Mechanical Vibrations

Forced Vibration Systems

Philadelphia University

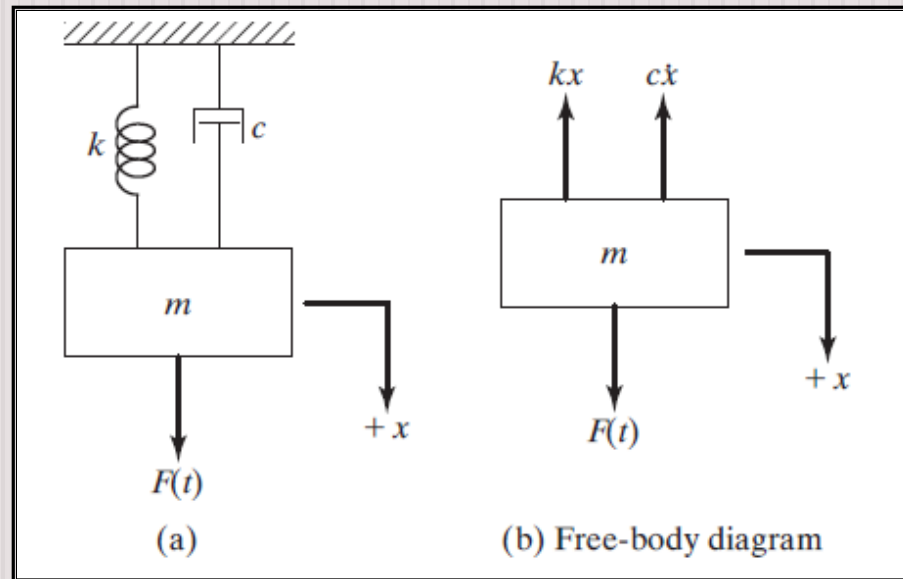
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Harmonically Excited Vibration

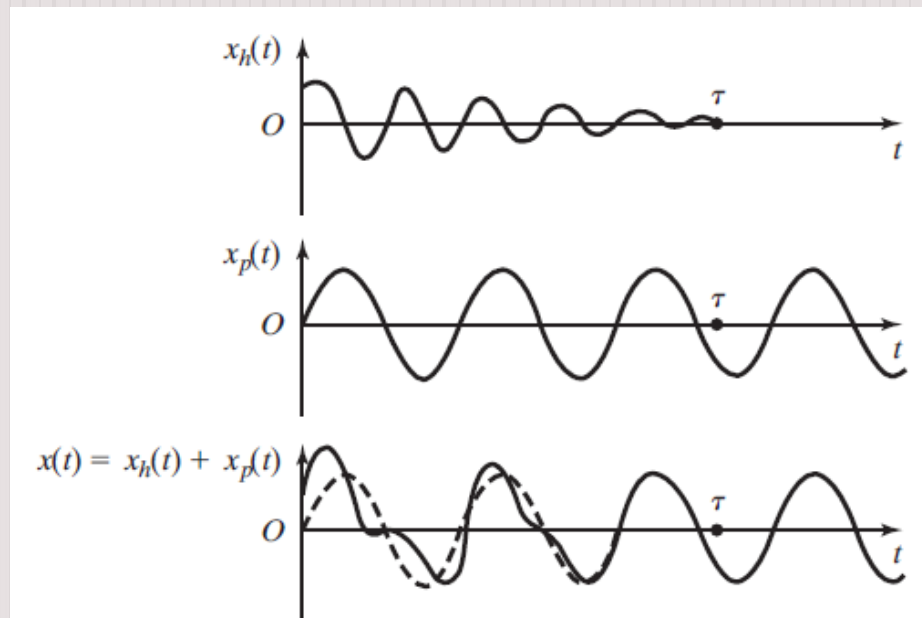
- Physical system



- Equation of motion: $m\ddot{x} + c\dot{x} + kx = F(t)$
- This equation is none – homogenous ODE
- The solution of this equation involves the solution of the homogenous part (discussed in the Ch.2) and a particular solution

Harmonically Excited Vibration

- Homogenous part of mathematical model represents a free vibration damped system: $m \ddot{x} + c \dot{x} + kx = 0$
- As seen from the previous discussion for this type of vibration, the amplitude will eventually die out.
- For steady state study of forced vibration, the particular solution is the only solution remains in the seen.



Un-damped Forced Vibration System

- Un-damped system: $m\ddot{x} + kx = F(t)$
- Because the main cause of forced vibration in rotating machinery is the unbalance, the most convenient and simple form of forcing vibration $F(t) = F_o \cos(\omega t)$. So, the governing equation become: $m\ddot{x} + kx = F_o \cos(\omega t) \dots \text{Eq.1}$
- The homogenous solution (Free vibration):
$$x(t) = C_1 \cos(\omega_n t) + C_2 \sin(\omega_n t)$$
- to find the particular solution, assume: $x_p(t) = X \cos(\omega t) \dots \text{Eq.2}$
where: X is constant that donates the maximum amplitude of $x_p(t)$.

Un-damped Forced Vibration System

- Substitution of Eq.2 into Eq.1 to find X:
$$X = \frac{F_o}{k - m\omega^2} = \frac{\delta_{st}}{1 - \left(\frac{\omega}{\omega_n}\right)^2}$$

where: $\delta_{st} = F_o/k$ denotes the deflection of mass (m) under the force F_o and it is called *static deflection*.

- The general solution now become:

$$x(t) = C_1 \cos(\omega_n t) + C_2 \sin(\omega_n t) + \frac{F_o}{k - m\omega^2} \cos(\omega t)$$

- using the I.Cs:

$$x(t=0) = x_o \Rightarrow C_1 = x_o - \frac{F_o}{k - m\omega^2}$$

$$\dot{x}(t=0) = \dot{x}_o \Rightarrow C_2 = \frac{\dot{x}_o}{\omega_n}$$

Un-damped Forced Vibration System

- Substitution C_1 and C_2 in the general solution:

$$x(t) = x_o - \frac{F_o}{k - m\omega^2} \cos(\omega_n t) + \frac{\dot{x}_o}{\omega_n} \sin(\omega_n t) + \frac{F_o}{k - m\omega^2} \cos(\omega t)$$

- The ratio between maximum amplitude and the static deflection (X/δ_{st}) can be expressed as:

Magnification factor

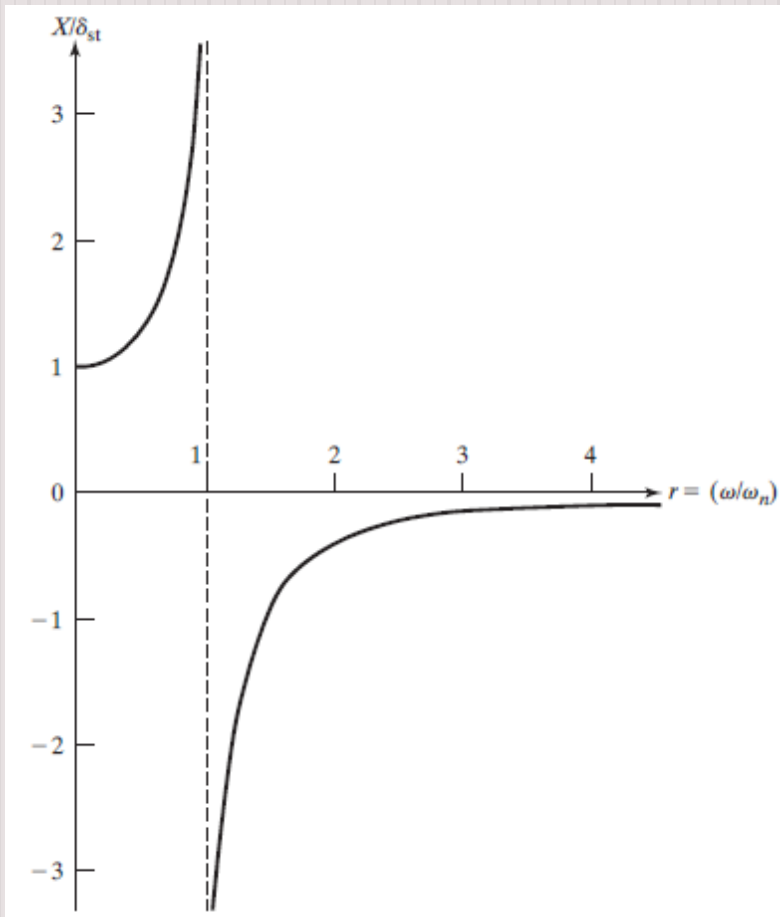
$$\frac{X}{\delta_{st}} = 1 / \left(1 - \left(\frac{\omega}{\omega_n} \right)^2 \right) = 1 / (1 - r^2)$$

Frequency ratio

- As you can see, there are three possible cases:
 - When $0 < r < 1$
 - When $r > 1$
 - When $r = 1$. this case is called resonance and the amplitude of vibration approaches the infinity.

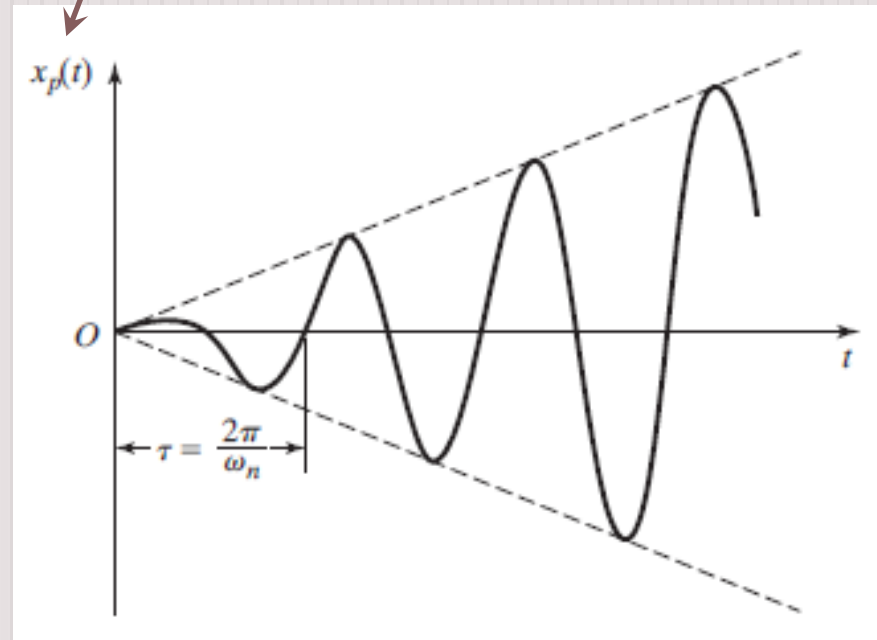
Resonance

All cases:



At resonance

Particular solution



Un-damped Forced Vibration System

Total response:

Homogenous solution

$$x(t) = A \cos(\omega_n t - \phi) + \frac{\delta_{st}}{1 - r^2} \cos(\omega t) \quad \text{for } r < 1$$

$$x(t) = A \cos(\omega_n t - \phi) - \frac{\delta_{st}}{r^2 - 1} \cos(\omega t) \quad \text{for } r > 1$$

- A and ϕ can be determined as in the previous analysis of free vibration:**

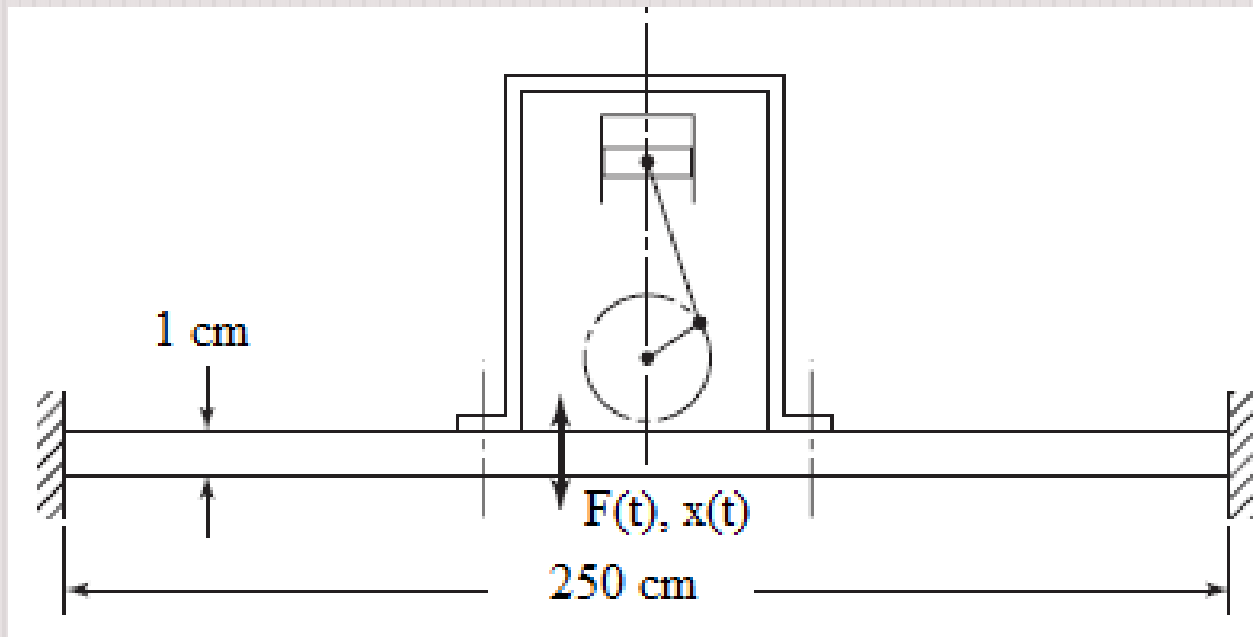
$$A = \sqrt{C_1^2 + C_2^2} = \sqrt{\left(x_o - \frac{F_o}{k - m\omega^2}\right)^2 + \left(\frac{\dot{x}_o}{\omega_n}\right)^2}$$

$$\phi = \tan^{-1}\left(\frac{C_2}{C_1}\right) = \tan^{-1}\left(\frac{\dot{x}_o / \omega_n}{x_o - F_o / k - m\omega^2}\right)$$

Un-damped Forced Vibration System

• Example 3.1: Plate Supporting a Pump:

A reciprocating pump, weighing 68 kg, is mounted at the middle of a steel plate of thickness 1 cm, width 50 cm, and length 250 cm. clamped along two edges as shown in Fig. During operation of the pump, the plate is subjected to a harmonic force, $F(t) = 220 \cos(62.832t)$ N. if $E=200$ Gpa, *Find the amplitude of vibration of the plate.*



Un-damped Forced Vibration System

- **Example 3.1: solution**

- **The plate can be modeled as fixed – fixed beam has the following stiffness:**

$$k = \frac{192EI}{l^3}$$

$$\text{But } I = \frac{1}{12}bh^3 = \frac{1}{12}(50 \times 10^{-2})(1 \times 10^{-2})^3 = 41.667 \times 10^{-9} \text{ m}^4$$

$$\text{So, } k = \frac{192(200 \times 10^9)(41.667 \times 10^{-9})}{(250 \times 10^{-2})^3} = 102,400.82 \text{ N/m}$$

- **The maximum amplitude (X) is found as:**

$$X = \frac{F_o}{k - m\omega^2} = \frac{220}{102,400.82 - 68(62.832)} = -1.32487 \text{ mm}$$

-ve means that the response is out of phase with excitation

Damped Forced Vibration System

- **Damped system:** $m \ddot{x} + c \dot{x} + kx = F_o \cos(\omega t)$
- **To find the particular solution, assume:** $x_p(t) = X \cos(\omega t - \phi)$.
- **Substitute the assumed solution into the governing equation and rearrange the terms:**

$$X \left[(k - m\omega^2) \cos(\omega t - \phi) - c\omega \sin(\omega t - \phi) \right] = F_o \cos(\omega t)$$

- **Use the trigonometric relations**

$$\cos(\omega t - \phi) = \cos(\omega t) \cos(\phi) + \sin(\omega t) \sin(\phi)$$

$$\sin(\omega t - \phi) = \sin(\omega t) \cos(\phi) - \cos(\omega t) \sin(\phi)$$

- **Therefore:**

$$X \left[(k - m\omega^2) \cos(\phi) + c\omega \sin(\phi) \right] = F_o$$

$$X \left[(k - m\omega^2) \sin(\phi) - c\omega \cos(\phi) \right] = 0$$

- **Solve for X and ϕ :** $X = \frac{F_o}{\sqrt{(k - m\omega^2)^2 + (c\omega)^2}} \quad \phi = \tan^{-1} \left(\frac{c\omega}{k - m\omega^2} \right)$

Damped Forced Vibration System

- Divide this equation $X = \frac{F_o}{\sqrt{(k - m\omega^2)^2 + (c\omega)^2}}$ by k and make the following substitutions:

$$\omega_n = \sqrt{\frac{k}{m}} \quad \xi = \frac{c}{c_c} \quad \delta_{st} = \frac{F_o}{k} \quad r = \frac{\omega}{\omega_n}$$

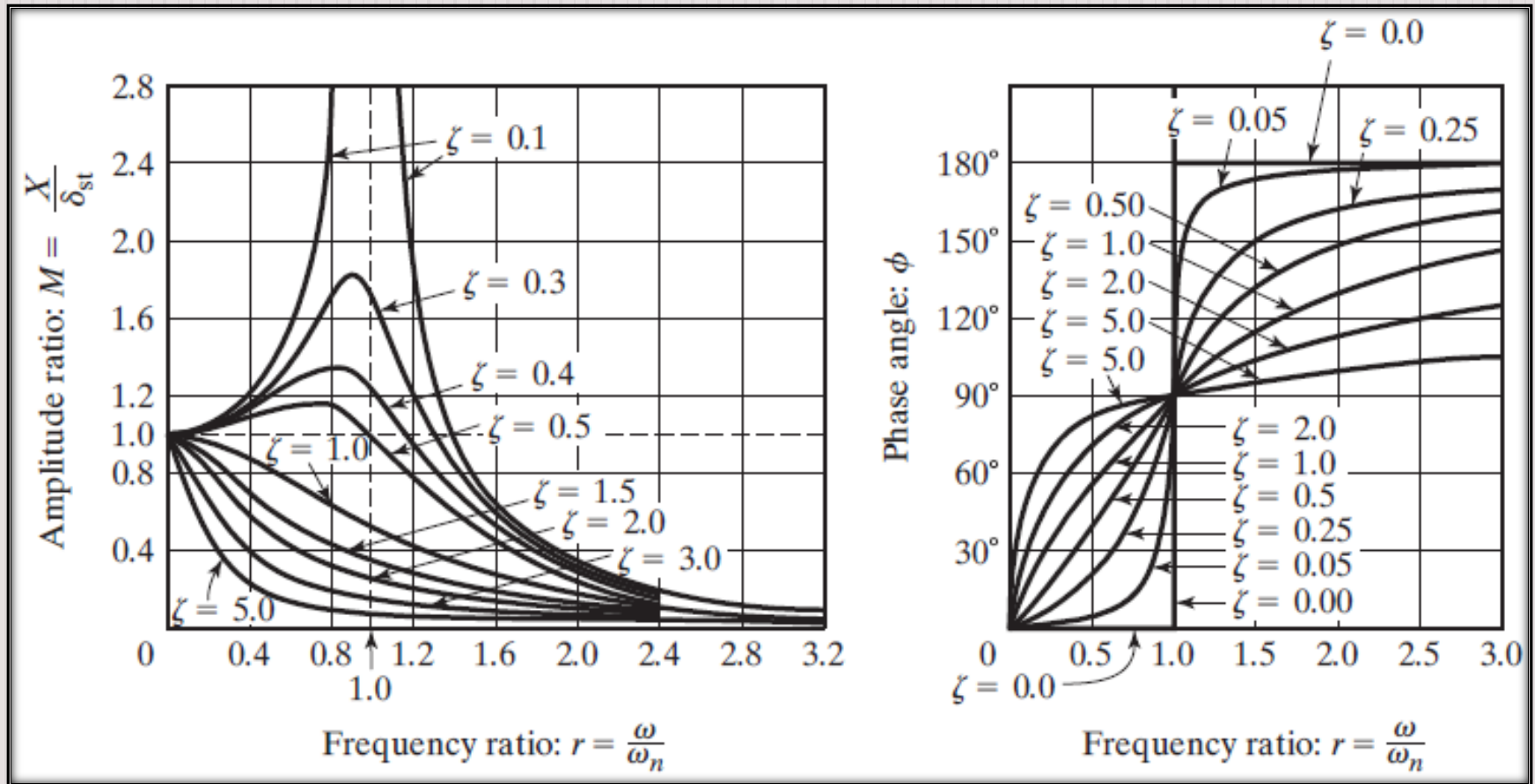
- You will eventually get:

$$\frac{X}{\delta_{st}} = \frac{1}{\sqrt{(1 - r^2)^2 + (2\xi r)^2}} \quad \text{and} \quad \phi = \tan^{-1}\left(\frac{2\xi r}{1 - r^2}\right)$$

Also called
amplitude ratio (M)

Damped Forced Vibration System

- Graphical representation for X and ϕ .



Damped Forced Vibration System

- Notes on the graphical representation for X .
 - ❑ For $\zeta = 0$, the system is reduced to become un-damped.
 - ❑ for any amount of (ζ) ; $\zeta > 0$, the amplitude of vibration decreases (i.e. reduction in the magnification factor M). This is correct for any value of r .
 - ❑ For the case of $r = 0$, the magnification factor equal 1.
 - ❑ The amplitude of the forced vibration approaches zero when the frequency ration approaches the infinity (i.e. $M \rightarrow 0$ when $r \rightarrow \infty$)

Damped Forced Vibration System

- Notes on the graphical representation for ϕ .
 - ❑ For $\zeta = 0$, the phase angle is zero for $0 < r < 1$ and 180° for $r > 1$.
 - ❑ For any amount of (ζ); $\zeta > 0$ and $0 < r < 1$, $0^\circ < \phi < 90^\circ$.
 - ❑ For $\zeta > 0$ and $r > 1$, $90^\circ < \phi < 180^\circ$.
 - ❑ For (ζ); $\zeta > 0$ and $r = 1$, $\phi = 90^\circ$.
 - ❑ For (ζ); $\zeta > 0$ and $r \gg 1$, ϕ approaches 180° .

Damped Forced Vibration System

Total response

- The total response is $x(t) = x_h(t) + x_p(t)$
- For under-damped system, the general solution is given as:

$$x(t) = X e^{-\xi \omega_n t} \{ \cos(\omega_d t - \phi) \} + X \cos(\omega t - \phi) \quad \text{where: } \omega_d = \sqrt{1 - \xi^2} \omega_n$$

- Assume the I.Cs: $x(t=0) = x_o$ and $\dot{x}(t=0) = \dot{x}_o$ and substitute it in the general solution:

$$\left. \begin{aligned} x_o &= X_o \cos(\phi_o) + X \cos(\phi) \\ \dot{x}_o &= -\xi \omega_n X_o \cos(\phi_o) + \omega_d X_o \sin(\phi_o) + \omega X \sin(\phi) \end{aligned} \right\} \text{--- Eq.1}$$

Damped Forced Vibration System

Total response

- Solve the Eq.1 to find X_o and ϕ_o :

$$X_o = \left[(x_o - X \cos(\phi))^2 + \frac{1}{\omega_d^2} \left(\xi \omega_n x_o + \dot{x}_o - \xi \omega_n X_o \cos(\phi_o) - \omega X \sin(\phi) \right)^2 \right]$$

$$\tan(\phi_o) = \frac{\left(\xi \omega_n x_o + \dot{x}_o - \xi \omega_n X_o \cos(\phi_o) - \omega X \sin(\phi) \right)}{\omega_d (x_o - X \cos(\phi))}$$

Damped Forced Vibration System

Example 3.2:

Find the total response of a single-degree-of-freedom system with $m = 10 \text{ kg}$, $c = 20 \text{ N-s/m}$, $k=4000 \text{ N/m}$, $x_o = 0.01\text{m}$ and $\dot{x}_o = 0$ under the following conditions:

- An external force $F(t) = F_o \cos(\omega t)$ acts on the system with $F_o = 100 \text{ N}$ and $\omega = 10 \text{ rad/sec}$
- Free vibration condition : $F(t) = 0$

Solution

a. From the given data

$$\omega_n = \sqrt{\frac{k}{m}} = \sqrt{\frac{4000}{10}} = 20 \text{ rad/s}$$

$$\xi = \frac{c}{2m\omega_n} = \frac{20}{2(10)(20)} = 0.05$$

$$\omega_d = \sqrt{1 - \xi^2} \omega_n$$

$$\omega_d = \sqrt{1 - 0.05^2} (20)$$

$$\omega_d = 19.975 \text{ rad/s}$$

$$r = \frac{\omega}{\omega_n} = \frac{10}{20} = 0.5$$

Damped Forced Vibration System

Example 3.2:

Solution

$$\delta_{st} = \frac{F_o}{k} = \frac{100}{4000} = 0.025m \longrightarrow X = \frac{\delta_{st}}{\sqrt{(1-r^2)^2 + (2\xi r)^2}} = 0.3326m$$

$$\phi = \tan^{-1}\left(\frac{2\xi r}{1-r^2}\right) = 3.814^\circ$$

• Using I.Cs to find X_o and ϕ_o

$$X_o = \left[(x_o - X \cos(\phi))^2 + \frac{1}{\omega_d^2} \left(\xi \omega_n x_o + \dot{x}_o - \xi \omega_n X_o \cos(\phi_o) - \omega X \sin(\phi) \right)^2 \right] = 0.0233$$

$$\tan(\phi_o) = \frac{\left(\xi \omega_n x_o + \dot{x}_o - \xi \omega_n X_o \cos(\phi_o) - \omega X \sin(\phi) \right)}{\omega_d (x_o - X \cos(\phi))} \Rightarrow \phi = 5.587^\circ$$

Damped Forced Vibration System

Example 3.2:

Solution

b. For free vibration: $x(t) = X e^{-\xi \omega_n t} \left\{ \cos\left(\sqrt{1-\xi^2} \omega_n t - \phi\right) \right\}$

$$X = \frac{\sqrt{x_o^2 \omega_n^2 + \dot{x}_o^2 + 2x_o \dot{x}_o \xi \omega_n}}{\sqrt{1-\xi^2} \omega_n} = 0.010012$$

$$\phi = \tan^{-1} \left[\frac{\dot{x}_o + \xi \omega_n x_o}{x_o \omega_n \sqrt{1-\xi^2}} \right] = 2.866^\circ$$

Substitute the values of X and ϕ into the general solution :

$$x(t) = 0.010012 e^{-t} \left\{ \cos(19.975t - \phi) \right\}$$

Base excitation

Example 3.2:

Solution

b. For free vibration: $x(t) = X e^{-\xi \omega_n t} \left\{ \cos\left(\sqrt{1 - \xi^2} \omega_n t - \phi\right) \right\}$

$$X = \frac{\sqrt{x_o^2 \omega_n^2 + \dot{x}_o^2 + 2 x_o \dot{x}_o \xi \omega_n}}{\sqrt{1 - \xi^2} \omega_n} = 0.010012$$

$$\phi = \tan^{-1} \left[\frac{\dot{x}_o + \xi \omega_n x_o}{x_o \omega_n \sqrt{1 - \xi^2}} \right] = 2.866^\circ$$

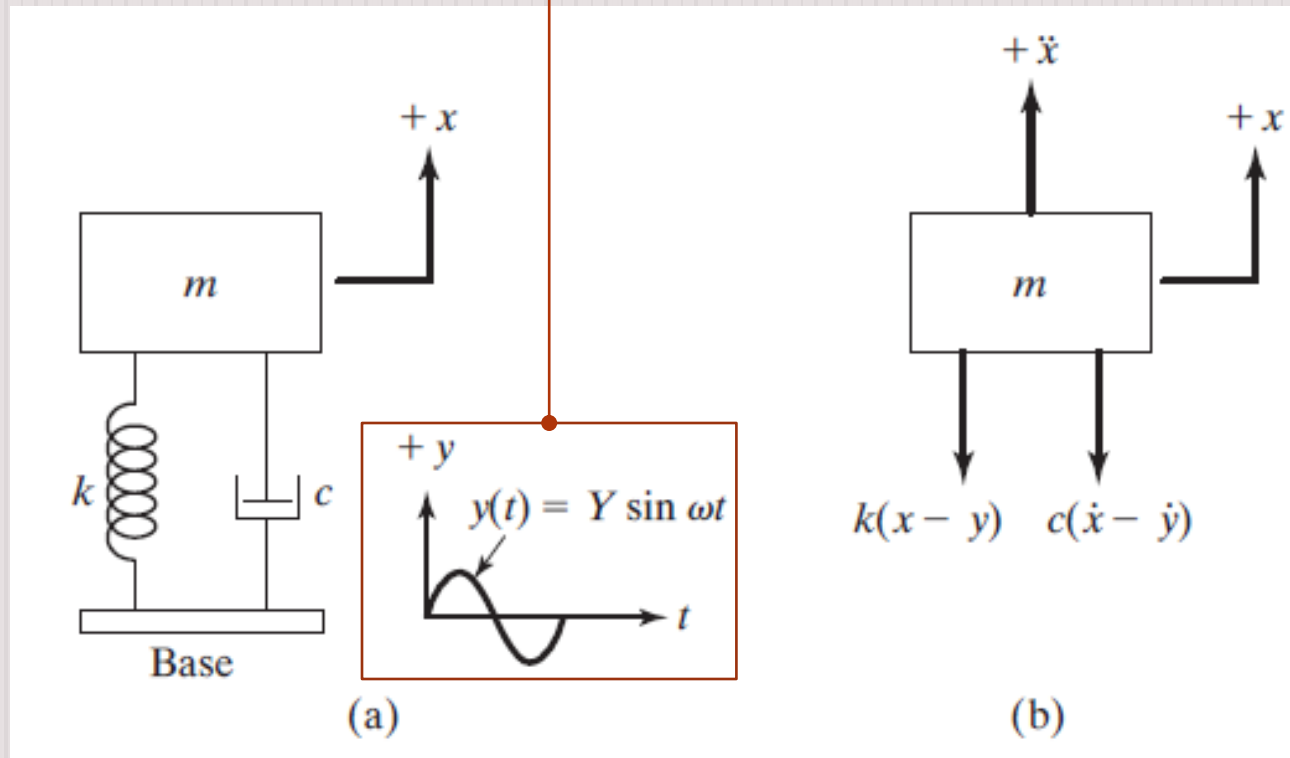
Substitute the values of X and ϕ into the general solution :

$$x(t) = 0.010012 e^{-t} \left\{ \cos(19.975t - \phi) \right\}$$

Forced Vibration System under Base Excitation

Physical system:

The forcing function for the base excitation



Mathematical model:
$$m \ddot{x} + c \left(\dot{x} - \dot{y} \right) + k(x - y) = 0$$

Forced Vibration System under Base Excitation

Substitute the forcing function into the math. Model:

$$m \ddot{x} + c \dot{x} + kx = kY \sin(\omega t) + c\omega Y \cos(\omega t) = A \sin(\omega t - \alpha)$$

Where:

$$A = Y \sqrt{k^2 - (c\omega)^2}$$

$$\alpha = \tan^{-1}\left(-\frac{c\omega}{k}\right)$$

This is harmonic excitation force

The particular solution: $x_p(t) = X \cos(\omega t - \phi)$.

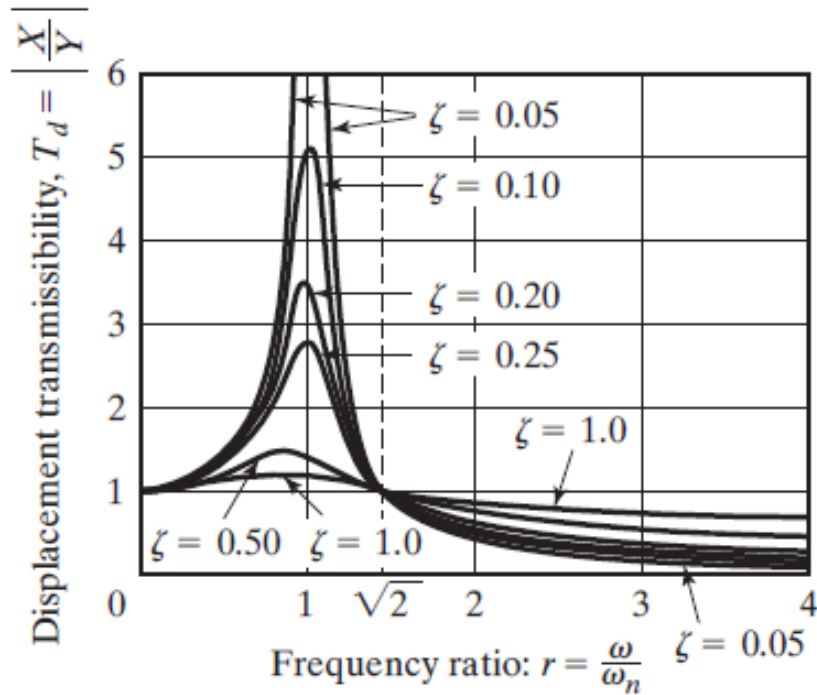
Displacement transmissibility

$$\frac{X}{Y} = \sqrt{\frac{k^2 + (c\omega)^2}{(k - m\omega^2)^2 + (c\omega)^2}} = \sqrt{\frac{1 + (2\xi r)^2}{(1 - r^2)^2 + (2\xi r)^2}}$$

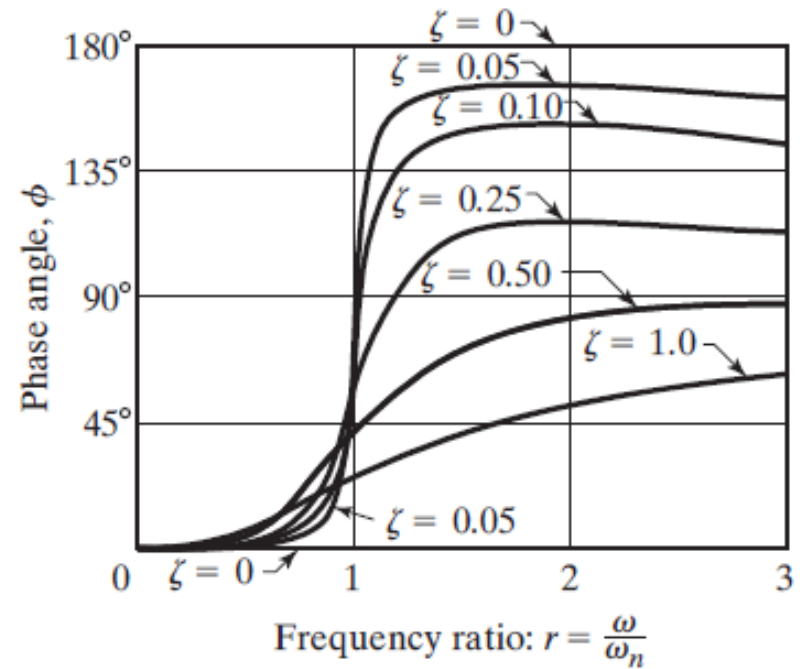
$$\phi = \tan^{-1}\left(\frac{mc\omega^3}{k(k - m\omega^2) + (c\omega)^2}\right) = \tan^{-1}\left(\frac{2\xi r^3}{1 + (4\xi^2 - 1)r^2}\right)$$

Forced Vibration System under Base Excitation

Graphical representation for X and ϕ .



(a)



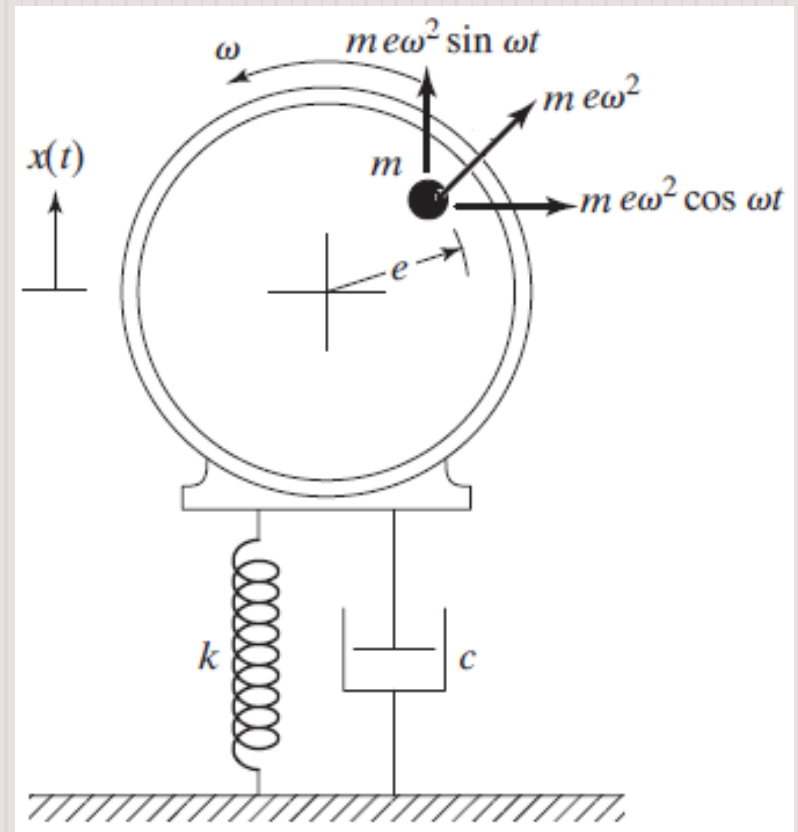
(b)

Forced Vibration System due to Unbalance

Assume the following general case:

- The centrifugal force equal $me\omega^2$
- The vertical component ($me\omega^2 \sin(\omega t)$) is the effective one because the direction of motion is vertical.
- the vertical component can be moved to the center of rotation due to vector definition.
- The equation of motion can derived as: $m\ddot{x} + c\dot{x} + kx = me\omega^2 \sin(\omega t)$
- The derived equation of monition is

a harmonic excited vibrating system which discussed before.



Forced Vibration System General Periodic force

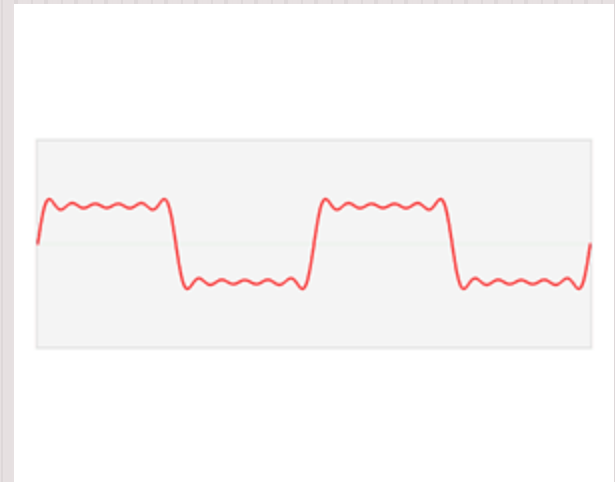
- In some cases, the external force $F(t)$ is periodic with period: $\tau = 2\pi / \omega$.
- Periodic force can expanded in Fourier series as:

$$F(t) = \frac{a_0}{2} + \sum_{j=1}^{\infty} a_j \cos(j\omega t) + \sum_{j=1}^{\infty} b_j \sin(j\omega t)$$

Where:

$$a_j = \frac{2}{\tau} \int_0^{\tau} F(t) \cos(j\omega t) dt$$

$$b_j = \frac{2}{\tau} \int_0^{\tau} F(t) \sin(j\omega t) dt$$



- The order of the expansion is (j)
- As the number of terms increases, as the accuracy of expanding increases.